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### Article

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# AC RTN: Testing, Modelling, and Prediction

Kean H. Tok, Jian F. Zhang, James Brown, Zengliang Ye, Zhigang Ji, Weidong Zhang, and John S. Marsland

**Abstract**— Random Telegraph Noise (RTN) adversely induces time dependent device-to-device variations and requires modelling to optimize circuit design. Many early works were focused under DC test conditions, although digital circuits typically operate under AC conditions and it has been reported that AC RTN is substantially different from DC RTN. Tests on AC RTN were carried out mainly on individual traps and a reliable statistical distribution of trap time constants for AC RTN is still missing. This prevents verifying the statistical accuracy of Monte Carlo AC RTN simulation based on compact models, especially in terms of their ability to predict AC RTN as time window increases. Recently, an integral methodology has been proposed for DC RTN, which can not only model it at short time, but also predict it at long time. By introducing the concept of effective charged traps, the need for statistical distribution of trap time constants is removed, making RTN prediction similar to ageing prediction. The objectives of this work are to report statistical experimental AC RTN data and to test the applicability of integral methodology to them. For the first time, it will be shown that a model extracted from a time window of 7.8 s can be used to predict the statistical distribution of long term ( $3 \times 10^4$  sec) AC RTN. The dependence of AC RTN on frequency and time window is analyzed and the contributions of carrier tunneling from gate and substrate are assessed.

**Index Terms**— Noise, Random telegraph noise (RTN), Jitters, Yield, Fluctuation, Device Variations, Time-dependent Variations.

## I. INTRODUCTION

RANDOM telegraph noise (RTN) in MOSFETs is caused by capturing a charge carrier from conduction channel and then giving it back [1]-[24]. It has attracted increasing amount of attentions recently, because of several reasons. First, the impact of a trapped charge increases as devices become smaller. Second, RTN is highly stochastic and induces a large time dependent device-to-device variation (DDV) and DDV has become a key issue for circuit design with nanoscale devices. Third, the need for low power consumption is driving operation voltage towards threshold,  $V_{th}$ , where a single trapped charge can have a large impact [1]-[5].

To assess the impact of RTN on circuits and to optimize their design, many efforts were made on both characterizing and modelling RTN [1]-[24]. On characterization, many early works were carried out under DC conditions [1],[6]-[15], although digital circuits typically operate under AC conditions. It has been reported that AC RTN is considerably different from DC RTN [16]-[19]. On modelling, works were carried out in

both time [2]-[11],[16]-[19] and frequency [22] domain. In the time domain, Monte Carlo simulation has been carried out for both DC and AC RTN by assuming that RTN transitions are memoryless random Markov process [16]-[21]. The required inputs are the statistical distributions of (i) trap capture ( $\tau_C$ )/emission ( $\tau_E$ ) time constants, (ii) RTN amplitude per trap, and (iii) number of traps per device. For AC RTN,  $\tau_C$  and  $\tau_E$  under both high ('H') gate bias  $V_g=V_{dd}$  and low ('L')  $V_g=0$  are needed, which are represented by  $\tau_{CH}$ ,  $\tau_{EH}$ ,  $\tau_{CL}$ , and  $\tau_{EL}$ , hereafter.

It is widely accepted that the number of traps per device follows the Poisson's distribution [23],[24]. It has been proposed that trap amplitude can follow Exponential [5],[16],[23], Log-normal [1],[6],[16], or Generalized Extreme Value (GEV) distribution [7],[24]. The time constants have been assumed to follow either Log-normal [8],[9] or Log-uniform [1],[10],[11] distributions. When compared with the amplitude distribution, there are less data available to underpin the  $\tau_C$  and  $\tau_E$  distribution, as they are difficult to collect in large numbers even for DC RTN. For AC RTN, there are more challenges: as transistor is switched off under  $V_g=0$ ,  $\tau_{CL}$  and  $\tau_{EL}$  cannot be measured directly.

Several methods were used to overcome the challenge and to obtain  $\tau_{CL}$  and  $\tau_{EL}$ . One of them is to assume that  $\tau_{CL}/\tau_{CH}$  and  $\tau_{EH}/\tau_{EL}$  is a constant, so that  $\tau_{CL}$  and  $\tau_{EL}$  can be estimated from the measured  $\tau_{CH}$  and  $\tau_{EH}$ , but the simulation results based on this assumption did not agree well with test data [8]. Another method uses compact models and  $\tau_C$  and  $\tau_E$  are assumed to be exponentially related to  $E_f-E_t$ , where  $E_f$  is the Fermi-level at dielectric/substrate interface and  $E_t$  is trap energy level [1],[3],[4],[19],[20].  $E_f-E_t$  under  $V_g=0$  can be calculated and it can then be used to evaluate  $\tau_{CL}$  and  $\tau_{EL}$ . The problem is that the time constants obtained in this way are not verified by test data, so that the accuracy of these compact models for AC RTN simulation is typically not known.

To provide experimental data for AC RTN, the measured data under  $V_g=V_{dd}$  were joined together by removing the time of  $V_g=0$  [17]. On one hand, it was reported that the  $\tau_C$  measured in this way changes little from its DC value. As  $\tau_{CL}$  is typically much larger than  $\tau_{CH}$ , the duration of  $V_g=0$  contributes little to trap capture and its removal has little effects on capture. On the other hand,  $\tau_{EL}$  is typically smaller than  $\tau_{EH}$ , so that the time under  $V_g=0$  can reduce the measured  $\tau_E$ . By measuring both  $\tau_C$  and  $\tau_E$  under  $V_g=V_{dd}$  and removing the  $V_g=0$  duration, the AC

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RTN of individual traps has been modelled successfully [16]-[19]. At present, however, there is a lack of reliable statistical distribution of the  $\tau_C$  and  $\tau_E$  measured in this way. As a result, the statistical accuracy of Monte Carlo modelling for AC RTN remains to be verified for multiple traps and devices in real circuits, especially in term of its capability to predict the AC RTN beyond the test time window.

The objectives of this work are threefold: to provide statistical AC RTN data at device level, rather than single trap; to develop a model for AC RTN, that can not only fit test data, but also predict the long term AC RTN; and to analyze test data and simulation results, leading to an improved understanding of AC RTN. Unlike the early works that focus on individual traps [17]-[19], AC RTN data with time window up to  $3 \times 10^4$  sec are collected on device level that can have multiple traps.

Recently, an integral methodology has been proposed and used to model DC RTN [24]. The applicability of this methodology to AC RTN will be tested in this work. The dependence of AC RTN on frequency and time window will be analyzed. Both acceptor-like and donor-like traps are modelled and their differences in carrier tunneling will be studied.

## II. DEVICES AND EXPERIMENTS

### A. Devices

nMOSFETs fabricated by a 28 nm CMOS process were used in this work. The channel width and length are 90 nm and 27 nm, respectively. The gate dielectric consists of a stack of a Hf-high-k layer and an interfacial SiON layer with an equivalent oxide thickness of 1.2 nm. The devices were arranged in arrays and each of them is assessed through address codes. The average threshold voltage,  $V_{th}$ , is 0.45 V.

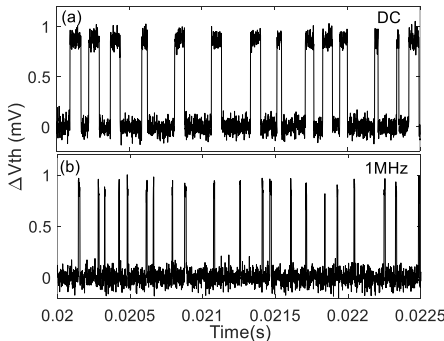


Fig. 1. An example of measured data for a device with one acceptor-like trap.  $V_g$  is under DC (a) and 1 MHz (b). The duration of  $V_g=0$  was removed in (b).

### B. Experiments

The tests were carried out with  $V_g$  alternating between 0.5 V and 0 V under a constant drain bias of 0.1 V. The top  $V_g$  is chosen to be close to  $V_{th}$  to make the test relevant to low power operation, where RTN can be profound [7],[10],[24]. The frequency of  $V_g$  is in a range of 100 Hz to 1 MHz with a duty cycle of 50%. Temperature is 125 °C. To enable statistical analysis, 402 devices were tested for a relatively short time window of 7.8 sec (time after removing  $V_g=0$  duration). To verify that the AC RTN model extracted from data in this short window can be used to predict long term RTN, tests with a time window up to  $3 \times 10^4$  sec were also carried out for 60 devices.

Before RTN test, a pulse (3  $\mu$ s) Id- $V_g$  was measured. During RTN tests, drain current, Id, was monitored continuously at a sampling rate of 1 Mpoint/sec [25]. The reference Id,  $I_{ref}$ , was obtained from the average of the first 10 points and the threshold voltage shift is evaluated from  $\Delta V_{th}=(I_{ref}-I_d)/g_m$ , where  $g_m$  is the transconductance obtained from the pulse Id- $V_g$  for each device at  $V_g=0.5$  V [24].

## III. RESULTS AND DISCUSSIONS

### A. AC RTN data at device level

When there is only one trap in a device, Figs. 1(a) and 1(b) compares the DC and AC RTN. Following the earlier works [17]-[19], the duration of  $V_g=0$  was removed in Fig. 1(b). We will use the term of ‘time’ or ‘time window’ for the cumulative time under  $V_g=0.5$  V, hereafter. For a duty cycle of 50%, the actual AC RTN test time doubles the ‘time window’. Under AC, the trap in Fig. 1 spends more time at the low level of  $\Delta V_{th}$  and there are more transitions between the two levels, in agreement with early work [17]. The result supports that this trap is acceptor-like, which captures an electron and induces a positive  $\Delta V_{th}$ . Because emission under  $V_g=0$  is more efficient, the trap can only hold the electron for short time at the high level of  $\Delta V_{th}$  in Fig. 1(b).

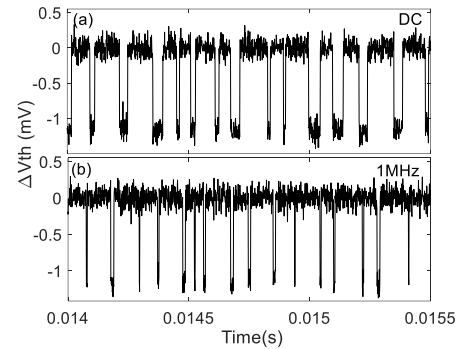


Fig. 2. An example of measured data for a device with one donor-like trap.  $V_g$  is under DC (a) and 1 MHz (b). The duration of  $V_g=0$  was removed in (b).

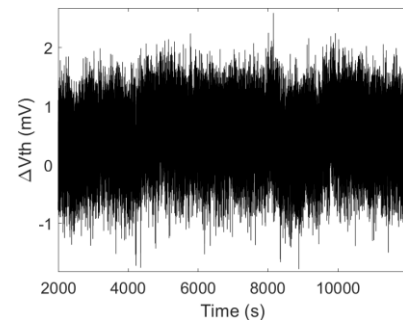


Fig. 3. An example of complex RTN over a long time window.

The positive  $\Delta V_{th}$  in Figs. 1(a) and 1(b) corresponds to a reduction of drain current, Id. An increase of Id was also often observed, which lead to a negative  $\Delta V_{th}$ , as shown in Figs. 2(a) and 2(b). This negative  $\Delta V_{th}$  can come from either charging a donor-like trap positively or emitting an electron from a prefilled acceptor-like trap. Following early work [24], we use the term ‘donor-like trap’ to represent  $\Delta V_{th}<0$ , hereafter. For AC RTN, Fig. 2(b) confirms that the emission of positive charge, i.e. capturing an electron and becoming neutral, is also more efficient under  $V_g=0$ .

The devices in Figs. 1 and 2 only have one active trap within the measurement window. The trap time constant in this case can be readily extracted and used for Monte Carlo simulation. Many devices, however, do not have such clear RTN signal. As time window increases, the number of active traps in a device increases, resulting in complex fluctuation and one example is given in Fig. 3. It is difficult to extract time constants of individual traps in this case. An integral methodology has been proposed to overcome this challenge [24] and will be briefly described next.

### B. Integral methodology

This method uses the  $\Delta V_{th}$  measured at device level as inputs and does not require experimentally separating  $\Delta V_{th}$  into contributions of individual traps. As a result, it does not require one device having only one trap and is applicable to devices with any number of traps. At a given time,  $\Delta V_{th}$  measured from multiple devices were grouped together to form a dataset and their cumulative distribution function (CDF) is given in Fig. 4. The concept of ‘Effective Charged Traps (ECT)’ is introduced, which assume that this CDF comes from a set of traps that are always charged. In this way, the burden for finding the statistical distribution of trap time constants is removed, greatly simplifying the testing and analysis.

The next step is to extract the number of ECT that can reproduce a given CDF of  $\Delta V_{th}$ . By assuming the number of traps per device follows the Poisson’s distribution and selecting a RTN amplitude distribution, such as Exponential, Log-normal, or GEV, the average number of ECT per device can be extracted by the maximum likelihood estimation for both acceptor-like ( $N_A$ ) and donor-like ( $N_D$ ) traps [24].

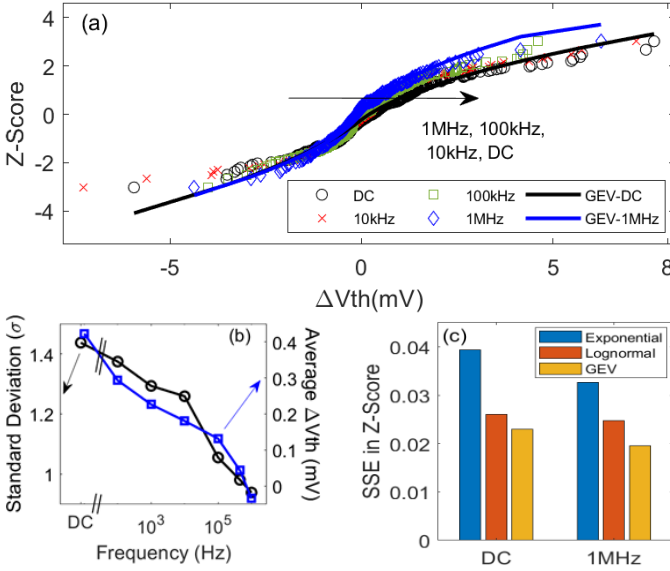


Fig. 4. (a) The Cumulative Distribution (CD) of test data (symbols). The lines are fitted function with GEV for DC (black) and 1 MHz (blue). (b) Dependence of standard deviation ( $\sigma$ ) and mean  $\Delta V_{th}$  on frequency. (c) A comparison of the sum of squared error (SSE) per device of the CDF extracted for DC and 1 MHz RTN. The RTN amplitude distribution per trap is assumed to follow Exponential, Log-normal, and GEV, respectively. The time window is 7.8 s.

The above process for extracting  $N_A$  and  $N_D$  is repeated for different time window. Longer time window covers slower traps and increases  $|\Delta V_{th}|$ , which in turn results in larger  $N_A$  and  $N_D$ . The  $N_A$  and  $N_D$  versus time obtained in this way can be used

to extract their kinetics. For DC RTN, it has been shown that this kinetics can be used to predict  $N_A$  and  $N_D$  at longer time [24]. Once  $N_A$  and  $N_D$  are known, the probability for a device to have a specific  $\Delta V_{th}$  can be calculated.

Table I. The pdf formula and their extracted parameter values.  $\delta V_{th}$  is the threshold voltage shift per trap.

	PDF of $\delta V_{th}$	Acceptor	Donor
Exponential	$\frac{1}{\eta} e^{-\frac{\delta V_{th}}{\eta}}$	$\eta = 0.54$	$\eta = 0.49$
Lognormal	$\frac{1}{\delta V_{th} \theta \sqrt{2\pi}} e^{-\frac{(\ln(\delta V_{th}) - \epsilon)^2}{2\theta^2}}$	$\epsilon = -0.37$ $\theta = 0.14$	$\epsilon = -0.64$ $\theta = 0.16$
GEV	$\frac{1}{\beta} (k)^{\xi+1} e^{-k}$ $k = \left(1 + \xi \left(\frac{\delta V_{th} - \alpha}{\beta}\right)\right)^{\frac{1}{\xi}}$	$\xi = 0.32$ $\alpha = 0.41$ $\beta = 0.36$	$\xi = 0.36$ $\alpha = 0.29$ $\beta = 0.23$
Thermal	$\frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{1}{2}\left(\frac{\Delta V_{th}}{\sigma}\right)^2}$	Exponential, $\sigma = 0.09$ Lognormal, $\sigma = 0.13$ GEV, $\sigma = 0.11$	

### C. Applicability of Integral methodology to AC RTN

$\Delta V_{th}$  under different frequencies is compared in Figs. 4(a) and 4(b).  $\Delta V_{th}$ , its mean value and standard deviation is smaller for AC RTN, because of the enhanced emission during  $V_g=0$ . As a result, the RTN under AC operation cannot be modeled from DC RTN data and AC measurements have to be carried out. Since  $\Delta V_{th}$  can be either positive or negative, its mean value ( $<1$  mV) is much smaller than its standard deviation.

The lines in Fig. 4(a) are the fitted cumulative distribution function (CDF). Their corresponding probability distribution function (PDF) and the extracted  $\alpha$  model parameters are given in Table I. Fig. 4(c) shows that the error for AC is not larger than that for DC. As a result, it is concluded that the integral method is equally applicable for AC RTN. This is understandable: AC mainly impacts emission, but the integral methodology assumes CDF originating from ECT that are always charged and detailed emission process is not needed here.

The results in Fig. 4 were obtained for a time window of 7.8 s. The same procedure is applied for other time windows between  $10^{-4}$  s and 7.8 s and the extracted  $N_A$  and  $N_D$  are given in Fig. 5 for Exponential, Log-normal, and GEV RTN amplitude distributions. As expected, both  $N_A$  and  $N_D$  increased with time window, but decreased for higher frequency due to reduced trap occupancy.

Fig. 6 gives the extracted average threshold voltage shift per trap,  $\mu$ . Unlike the  $N_A$  and  $N_D$  in Fig. 5,  $\mu$  is insensitive to frequency. This is because that the same traps are responsible for AC and DC RTN. Although AC enhances emission, it does not change RTN amplitude, as shown in Figs. 1 and 2.

The  $N_A$  and  $N_D$  versus time in Fig. 5 can be used to extract their kinetics. Three different kinetics were tested: power law, scaled Log-normal CDF, and Log-uniform [24]. Fig. 5 shows that all three can fit the data reasonably well within the short time window of 7.8 s. One powerful feature of the integral methodology is that these kinetics can be extrapolated to longer time window to predict the long term DC RTN [24], making RTN prediction similar to predicting ageing induced by bias temperature instabilities [26],[27] and hot carriers [28]. The prediction capability for AC RTN will be tested next.

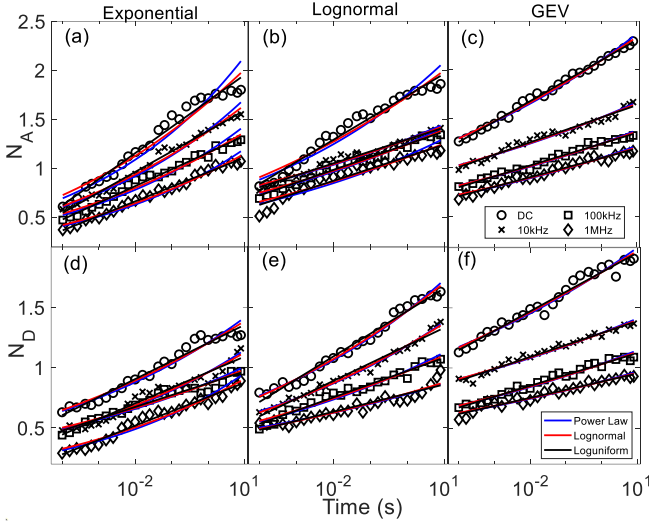


Fig. 5. Dependence of average number of ECT per device on time window (symbols) at different frequencies.  $N_A$  in the top row (a,b,c) is for acceptor-like traps with Exponential, Log-normal, and GEV distributions, respectively.  $N_D$  in the bottom row (d,e,f) is for donor-like traps. The lines are fitted kinetics with Power law (blue), scaled Log-normal CDF (red), and Log-uniform (black).

Fig. 7 gives the  $N_A$  and  $N_D$  for AC RTN measured up to a time window of  $3 \times 10^4$  sec. The three kinetics extracted from the data within 7.8 s is extrapolated and compared with the test data. The differences between predictions by the three kinetics can be considerable and some kinetics clearly agrees better with the test data. To make a quantitative comparison, Fig. 8 gives the errors between predictions and test data. When RTN amplitude is assumed to follow Exponential and Log-normal distribution, the scaled Log-normal CDF kinetics give lower errors. The lowest error, i.e. the best fit, however, is obtained for GEV with Log-uniform kinetics.

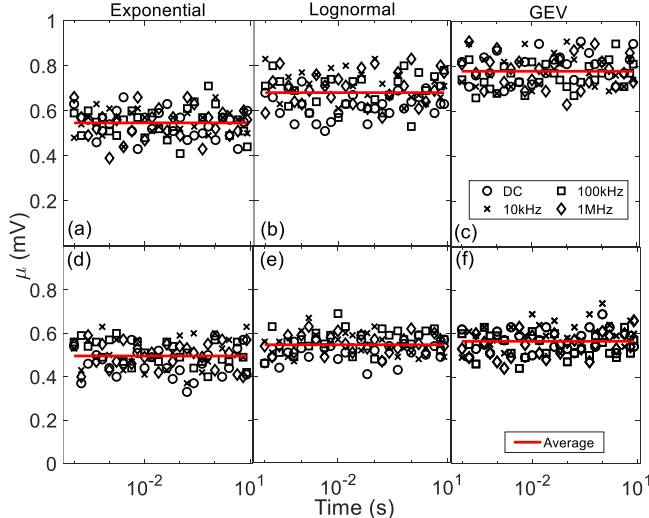


Fig. 6. The extracted average  $\delta V_{th}$  per trap,  $\mu$ , for DC and AC RTN at different frequencies. Solid lines are the mean values of all data. (a,b,c) are acceptor-like traps and (d,e,f) are donor-like traps.

We now investigate how well the  $N_A$  and  $N_D$  predicted in Fig. 7 can be used to evaluate the CDF at an AC time window of  $3 \times 10^4$  sec. Figs. 9(a) and 9(b) compares the CDF calculated from the predicted  $N_A$  and  $N_D$  with the measured one and good agreement has been obtained. Fig. 9(c) shows that the

prediction error for AC RTN is similar to that for DC RTN. As a result, the integral methodology can be used to extract a model from 7.8 s tests that is capable to predict AC RTN at  $3 \times 10^4$  sec, over three orders of magnitude ahead in time.

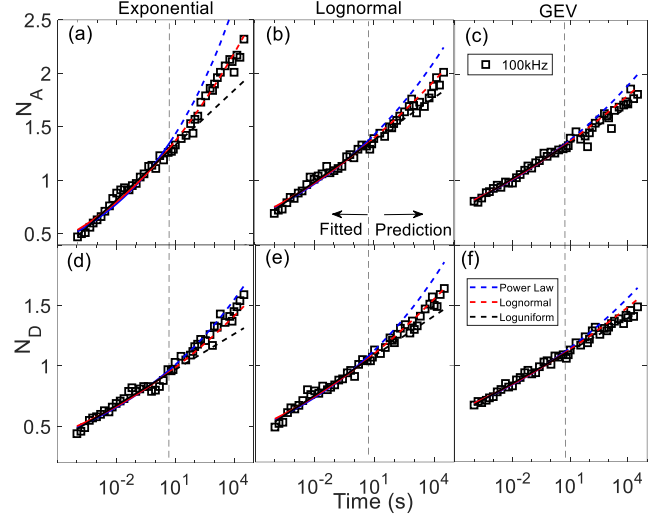


Fig. 7. Prediction of the average number of acceptor-like traps,  $N_A$ , in the top row (a, b, c) and donor-like traps,  $N_D$ , in the bottom row (d, e, f) for AC RTN at 100 kHz. Symbols are extracted by fitting the  $\delta V_{th}$  distributions (Exponential, Lognormal, and GEV). The solid lines within 7.8 s are the fitted kinetics with Power law (blue), Log-normal (red), and Log-uniform (black). The dashed lines beyond 7.8 s are extrapolated from the solid lines. The symbols beyond 7.8 s were not used for fitting.

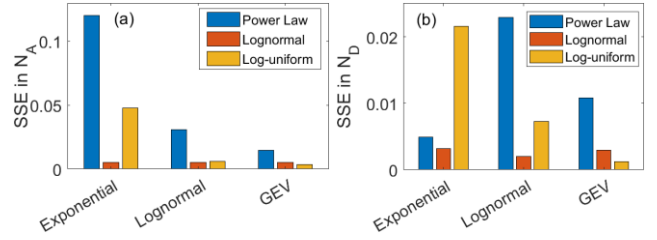


Fig. 8. The sum of squared errors per device of the prediction in Fig. 7 for acceptor-like (a) and donor-like (b) average number of traps per device. The lowest errors were obtained for Log-uniform kinetic with GEV  $\delta V_{th}$  distribution.

A comparison of Fig. 4(a) with Fig. 9(a) shows that their  $\Delta V_{th}$  has similar range. Figs. 4(a) and 9(a) were obtained for a time window of 7.8 and  $3 \times 10^4$  s, respectively. One would expect that Fig. 9(a) should have a larger  $\Delta V_{th}$  range, as larger time window allows slower traps to be included. This apparent discrepancy originates from the difference in number of samples used: 402 for Fig. 4(a) and 60 for Fig. 9(a). A larger number of samples has more chances of capturing rare event and, in turn, increases the statistical range. This compensates the effect of smaller time window.

#### D. Analysis of AC RTN

Fig. 10 shows  $N_A(AC)/N_A(DC)$  and  $N_D(AC)/N_D(DC)$  against time window. The main feature is that they decrease relatively fast with time initially and then more slowly for longer time window. For a given trap, its emission time follows [1],[3],[4],[19],[20],

$$\tau_E \propto \exp\left(\frac{E_f - Et}{kT}\right). \quad (1)$$

At a given distance from the interface, a trap with its energy level  $E_t$  further below  $E_f$  will have larger  $\tau_E$ . When  $V_g$  is switched from  $V_{dd}$  to zero for AC RTN, it shifts  $(E_f - E_t)$  by the same amount for traps of different  $E_t$ . This means  $\tau_{EL}/\tau_{EH}$  should be same for fast and slow traps, so that one may expect  $N_A(AC)/N_A(DC)$  to be independent of time window, against the observed reduction in Fig. 10. To understand the reduction in Fig. 10, we examine the impact of frequency on  $\tau_E$  next.

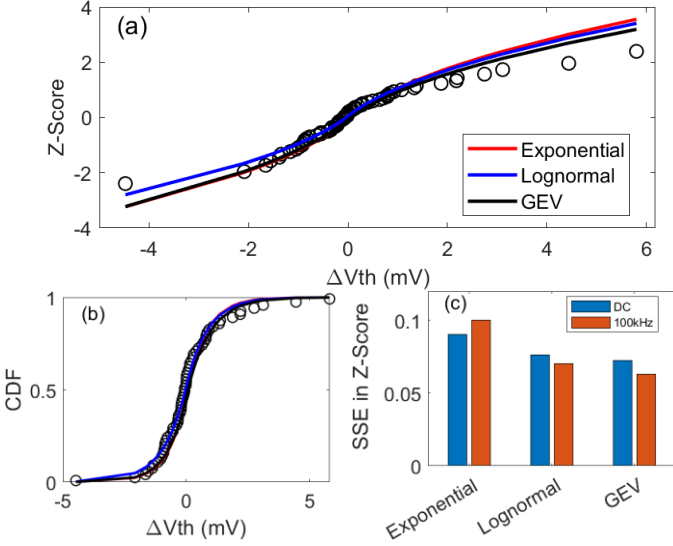


Fig. 9. AC (100 kHz) RTN prediction for the CDF of  $\Delta V_{th}$  at the time window of  $3 \times 10^4$  s by the model extracted from test data within 7.8 s. Symbols are the measured data and the lines are the calculated CDF by using the predicted  $N_A$  and  $N_D$  in Fig. 7 and the average  $\mu$  in Fig. 6, based on different  $\delta V_{th}$  distributions. The CDF is plotted in Z-score (a) and linearly in (b). (c) compares the errors of DC and AC predictions and shows that the smallest error was obtained for Log-uniform kinetic with GEV  $\delta V_{th}$  distribution.

When there is only one active trap in a device, like that in Figs. 1 and 2, its  $\tau_C$  and  $\tau_E$  can be readily extracted and one example for acceptor-like and donor-like trap is given in Fig. 11(a) and 11(b), respectively. In agreement with early work [16]-[19],  $\tau_C$  is independent of frequency,  $f$ , because  $\tau_{CL} \gg \tau_{CH}$  and removing the  $V_g=0$  durations have little impact on capture.

Although  $\tau_{EH}$  and  $\tau_{EL}$  are determined by  $(E_f - E_t)$  and should be independent of frequency, the  $\tau_E$  measured at  $V_{dd}$  in Figs. 1(b) and 2(b) is neither  $\tau_{EH}$  nor  $\tau_{EL}$  and Fig. 11 shows that it can depend on frequency, in agreement with early work [16]-[19]. The dependence of  $\tau_E$  on frequency can be divided into three regions. At low frequency Region 1 (R1) in Fig. 11,  $\tau_E$  is insensitive to frequency. In Region 2 (R2),  $\tau_E$  reduces for higher frequency. Finally, in high frequency Region 3 (R3),  $\tau_E$  becomes insensitive to frequency again. A physical interpretation for this dependence will be given below.

In the inset of Fig. 11(a),  $t_H = 1/(2f)$  is half of the AC period under  $V_g=0.5$  V. The number of RTN transition during  $t_H$ ,  $n$ , is:

$$n = \frac{2t_H}{\tau_{CH} + \tau_{EH}}, \quad (2)$$

In R1,  $f$  is low enough to make  $t_H \gg (\tau_{CH} + \tau_{EH})$ . There are many RTN transitions within  $t_H$ , i.e.  $n \gg 1$ . During  $V_g=0$ ,  $t_L \gg \tau_{EL}$ , but when  $t_L$  is removed by joining the two dots in Fig. 11(a) together, the number of emission will be increased by a maximum of 1 to  $(n+1) \approx n$ , so that the measured  $\tau_E \approx \tau_{EH}$ , which

is hardly affected by  $V_g=0$  duration and independent of frequency here.

As frequency increases and  $t_H$  reduces in R2,  $n$  approaches 1. If  $t_L \gg \tau_{EL}$ , trapped charge will be emitted during  $t_L$  and the number of emission during one AC period is  $(n+1) > n$ . The emission during  $t_L$  reduces the measured  $\tau_E$ . When  $n \ll 1$ ,  $(n+1) \approx 1$ , the measured  $\tau_E$  now is controlled by frequency and does not equal to  $\tau_{EH}$ . An increase of frequency reduces  $t_L$  and in turn  $\tau_E$ .

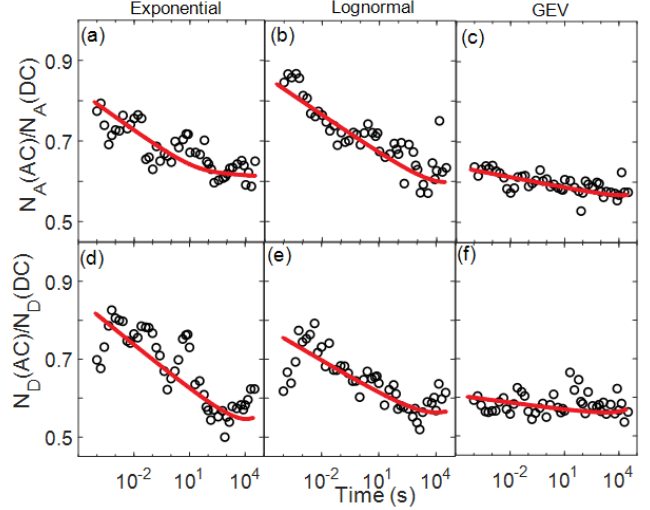


Fig. 10. AC (100 kHz) RTN against DC RTN ratio from  $10^{-4}$  to  $3 \times 10^4$  s for acceptor-like traps,  $N_A$ , in the top row (a, b, c) and donor-like traps,  $N_D$ , in the bottom row (d, e, f). The red lines are eye guides, showing that the reduction trend slows down at longer time.

Finally, when frequency is high enough to make  $t_L \ll \tau_{EL} < \tau_{EH}$ , we enter R3 where emission happens during both  $t_H$  and  $t_L$  to give,

$$\tau_E = \frac{\tau_{EH}\tau_{EL}}{\tau_{EH} + \tau_{EL}}. \quad (3)$$

$\tau_E$  now is independent of frequency again. If  $\tau_{EL} \ll \tau_{EH}$ ,  $\tau_E \approx \tau_{EL}$ , i.e. although the measurement is at  $V_g=V_{dd}$ , the measured  $\tau_E$  is actually the emission time at  $V_g=0$ .

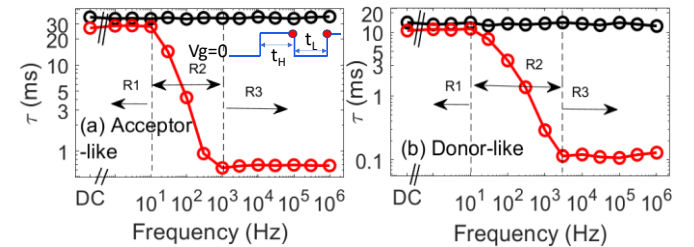


Fig. 11. Time constants,  $\tau$ , versus frequency for single acceptor-like trap (a) and donor-like trap (b). The red and black symbols are emission ( $\tau_E$ ) and capture ( $\tau_C$ ) time, respectively. R1, R2, and R3 are the three regions for the emission time.

We now use Fig. 11 to explain the results in Fig. 10. When time window is small, active traps are fast and they can be either in R1 or close to the top of R2, where AC reduces  $\tau_E$  modestly, resulting in a relatively large  $N_A(AC)/N_A(DC)$  in Fig. 10. As time increases, slower traps become active and they are in R2, where AC causes an increasingly larger reduction of  $\tau_E$ , leading to the reduction of  $N_A(AC)/N_A(DC)$ . As time increases further, the new active traps are slow enough to be in R3, where the impact of AC

on  $\tau_E$  stabilizes, so that  $N_A(AC)/N_A(DC)$  only decreases slowly with time here.

The test facilities used in this work only allows reliable measurement to be made up to 1 MHz. There are traps that are too fast to make  $\tau_L \ll \tau_{EL}$  even at 1 MHz, so that they do not enter R3. Examples of this case are given in Fig. 12(a) and 12(b) for acceptor-like and donor-like traps, respectively. This explains the continuous reduction of  $N_A$  and  $N_D$  with frequency in Fig. 13.

We now use the AC RTN to study the difference in tunneling process between acceptor-like and donor-like traps. For acceptor-like traps, emission will be more efficient under  $V_g=0$ , if electron is emitted to the substrate, as illustrated in Fig. 14a. The enhanced emission of AC RTN supports the tunneling is between traps and substrate, therefore.

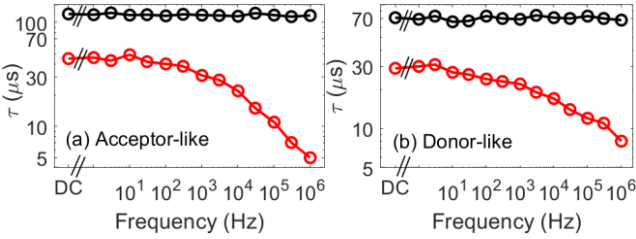


Fig. 12. Time constant,  $\tau$ , versus frequencies for single acceptor-like trap (a) and donor-like trap (b). In contrast with Fig. 11, the emission time does not enter into region R3 even at 1 MHz here.

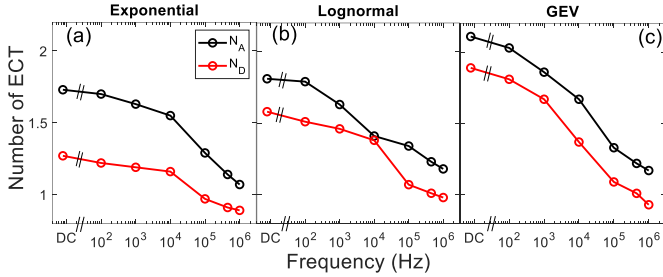


Fig. 13. Dependence of the extracted  $N_A$  (black) and  $N_D$  (red) at 7.8 s on frequency. (a,b,c) uses Exponential, Log-normal, and GEV  $\delta V_{th}$  distribution, respectively.

For donor-like traps, AC also enhances the emission, as shown in Figs. 2(b), 11(b) and 12(b). To neutralize the positive charge or to restore the pre-trapped electron, an electron must tunnel to the trap. If this electron comes from the substrate, it should be less efficient under  $V_g=0$  than under  $V_g=+0.5$  V, which disagrees with enhanced emission under AC. On the other hand, electron tunneling to the trap is more efficient under  $V_g=0$ , if it is from gate, as illustrated in Fig. 14b. As a result, acceptor-like and donor-like traps should be dominated by tunneling from substrate and gate, respectively. For a given time window, one may also expect that active donor-like traps are closer to the gate. This is supported by the smaller average impact per donor-like trap in Fig. 6. On the relative tunneling from gate against that from substrate, Figs. 14(c) and 14(d) shows  $N_D/N_A$  is around 0.8 and insensitive to either time or frequency.

#### IV. CONCLUSIONS

Unlike early works that focused on individual traps, this work reports statistical experimental data for AC RTN at device level with time window up to  $3 \times 10^4$  sec. The  $\Delta V_{th}$  measured from multiple devices were grouped together to form a data set

and it is found that the integral methodology is equally applicable to AC RTN as to DC RTN. At a given time, the CDF of  $\Delta V_{th}$  is used to extract the number of effective charged acceptor-like and donor-like traps through the maximum likelihood estimation. The  $N_A$  and  $N_D$  obtained from data within a time window of 7.8 s is used to extract their kinetics. For the first time, it is shown that these kinetics can predict the  $N_A$  and  $N_D$  at  $3 \times 10^4$  sec, a factor of 3,846 ahead in time. The CDF evaluated from the predicted  $N_A$  and  $N_D$  agrees well with test data. If one assumes that  $N_A$  and  $N_D$  kinetics extracted from a test time of one day can predict the AC RTN by the same factor of 3,846 ahead, it will cover a time range over 10 years. The dependence of AC RTN on time window and frequency is analyzed and RTN still reduces with frequency at 1 MHz, indicating there are traps with an emission time under  $V_g=0$  less than 1  $\mu$ s. The AC RTN data support that there are substantial tunneling activities between traps and both gate and substrate.

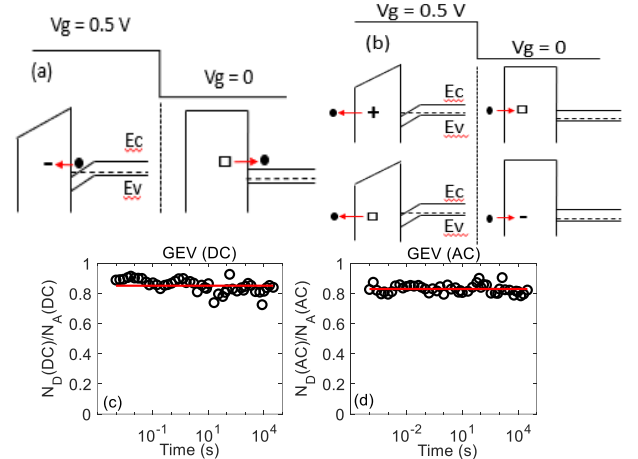


Fig. 14. A schematic illustration of carrier tunneling for acceptor-like trap (a) and donor-like trap (b) to explain the AC-enhanced emission.  $N_D/N_A$  is independent of time for both DC (c) and AC (d) RTN. ●, -, +, and □ represents electron, trapped negative, trapped positive charges, and neutral traps, respectively.

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