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A review of interconnection technologies for improved crystalline silicon solar cell photovoltaic module assembly

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Abstract

The identification, adoption and utilisation of reliable interconnection technology to assembly crystalline silicon solar cells in photovoltaic (PV) module are critical to ensure that the device performs continually up to 20 years of its design life span. With report that 40.7 % of this type of PV module fails at interconnection coupled with recent reports of increase in such failure in the tropics, the review of interconnection technologies employed in crystalline silicon solar cells manufacture has become imperative. Such review is capable of providing information that can improve the reliability of the system when adopted which in turn will increase silicon PV module production share more than the current value of 90.956%. This review presents the characteristics of interconnect contacts in conventional cells and other unconventional crystalline silicon cells. It compares series resistance, shadowing losses and the induced thermo-mechanical stress in the interconnection for each interconnection technique employed. The paper also reviews interconnection technologies in these assemblies and presents a comparison of their concept, cell type, joint type, manufacturing techniques and production status. Moreover, the study reviews and discusses the material and technological reliability challenges of silicon solar cells interconnection. The review identifies laser soldering technology as one which has the potential of making interconnection with higher reliability when compared with conventional soldering technology. It was found that this technology supports the current design trend of thinner, wider and cheaper crystalline silicon solar cells significantly whilst producing interconnection that experience relatively lower induced thermo-mechanical stress. The authors recommend that wider acceptance and usage of laser soldering technology could improve the performance and consequently extend the mean-time-to-failure (MTTF) of photovoltaic modules in general and particularly the ones which operates in the tropics. This will enable improvement in the reliability of PV modules for sustainable energy generation.

Keywords: *Photovoltaic modules; Crystalline silicon solar cells; Interconnection technology; Reliability*

1. Introduction

Photovoltaic (PV) modules constitute significant development in the worldwide green energy sector in the current campaign to increase sustainable energy production. Currently, the module is in huge demand because they are now used to supply electrical power [1, 2] to many applications. To meet the demand, the production of solar cells has increased because the modules are assembled by interconnecting solar cells to each other. It is expected that in the year 2020, the world annual production of solar cells will be around 100 GW_p (W_p, is peak power produced under standard test conditions). While this amount of sustainable power

47 production seems substantial, the continued operation of the module up to its design service
48 life has become a concern because the desired power generation is lower than expected.

49 The silicon solar cells have been identified as the most viable option suitable for large
50 volume production [3]. However, it has been reported that the continual generation of
51 electricity by PV modules, manufactured using this type of cell, in the field for a minimum
52 life span of 20 years has been a concern [1, 4-6]. One of the key challenges is untimely
53 failure of solar cells interconnection in the modules [7]. The interconnections provide
54 electrical, mechanical and thermal contact between the solar semiconductor cell and
55 electrodes.

56 The failure of the interconnection is caused by degradation of solder joints during module's
57 field operations due to temperature cycling. Extreme degradation often culminates in module
58 failure. The existence of this phenomenon and the need to provide solution has been reported
59 in [1, 6, 8-10]. The analysis of the failure mechanisms of PV modules in the field
60 demonstrates that the modules fail by many different modes. McCluskey [7] and Campeau, et
61 al [11] have reported that according to a BP study, 40.7% of PV module failures observed
62 were due to cell or interconnect breakage. This finding, in addition to other similar findings,
63 has identified the reliability of PV interconnections as the current challenge in PV modules
64 manufacture.

65 Consequently, the interconnection technologies of silicon PV modules were selected for
66 review. Silicon PV modules were chosen because the production of silicon-based solar cells
67 was 90% of all solar cells produced globally in 2008 [3]. This production share may have
68 been achieved because Silicon, being the second most abundantly available element on earth
69 [12], has been used as the primary feedstock. For instance, this largest share of production
70 was more than 90.956% of global PV module production in 2013 [13] and this share of
71 production is expected to remain for a long time. This paper explores and characterises
72 silicon solar cell interconnection technologies used in the various crystalline silicon solar cell
73 manufactures.

74 The objectives of this study are to present an overview of crystalline silicon PV modules
75 while dwelling on the characterisation of the solar cell contact and interconnection
76 technologies. The work advances to seek to review the current reliability challenges of the
77 interconnection of the solar cells with regards to interconnection technique. In addition, the
78 paper reviews research trends in solar cell interconnection and assembly technologies -
79 focusing on the identification of suitable technology to meet long-term reliability demand of
80 PV modules for energy generation.

81

82 **2. Crystalline silicon solar cells interconnection technologies**

83 The contact and interconnection technology of conventional wafer-based silicon solar cells
84 are discussed in sub-section 2.1 while challenges of conventional interconnection technology
85 are presented in sub-section 2.2. A comparison of conventional and unconventional
86 interconnection technologies is discussed in sub-section 2.3.

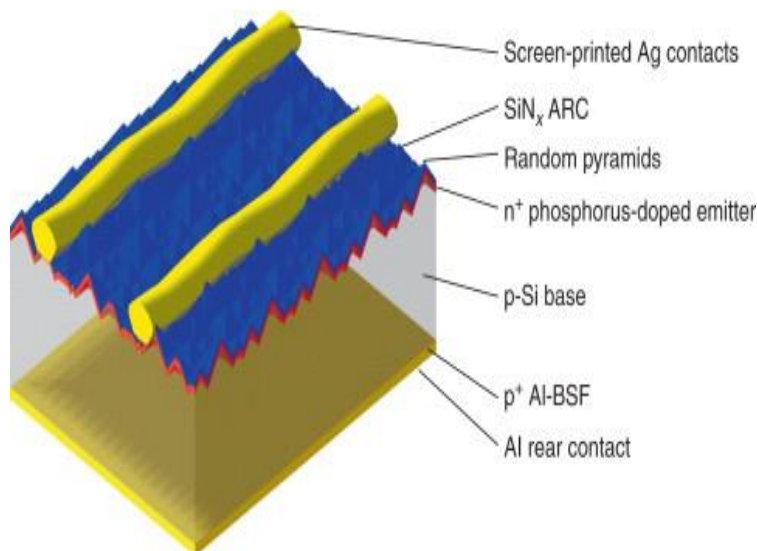
87 **2.1 Interconnection technology of conventional crystalline silicon solar cells**

88

89 The assembly and manufacturing process of conventional solar cells involves converting
90 silicon wafers into solar cells through depositing layers of emitter material and anti-reflection

91 coating (ARC). This process is followed by printing front metal electrode and back contacts
92 on the cell material as well as soldering of highly conductive solder-coated ribbon strip along
93 the length of the cell. An extended part of the ribbon strip is soldered to the back of a
94 neighbouring cell to enable current transfer from the front of one cell to the back of a
95 neighbouring cell in a series connection [5]. The use of low resistant electrode and finer lines
96 for a larger aperture in the manufacture enables the delivery of higher short circuit current
97 (I_{sc}) and fill factor to the ribbon strip [14]. The interconnection of solar cells in crystalline
98 silicon modules by soldering process is a high temperature process which occurs at about 250
99 °C. The elevated temperature soldering induces thermo-mechanical stress in the solder joints.

100
101 Metallization technologies in use for solar cells contact formation include: screen printing,
102 stencil-printing, pad-printing, ink-jet printing, dispensing technology, photolithographic and
103 evaporation process, laser micro-sintering, plating (Nickel) and thickening of metal contacts
104 by means of plating [15]. In the photovoltaic industry, the predominant technique used for the
105 establishment of an ohmic contact to an n-type emitter of a crystalline silicon solar cell is
106 screen printing of an Ag-based thick-film paste and firing through the ARC layer [15-18]. A
107 typical structure of Aluminium Back Surface Field (Al-BSF) solar cell is shown in Fig.1.



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110
111 Fig.1. Typical structure of Al-BSF solar cell [16]
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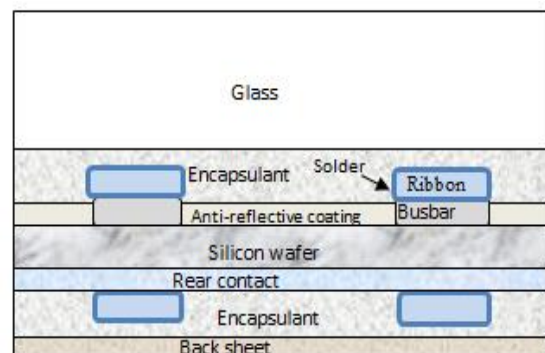
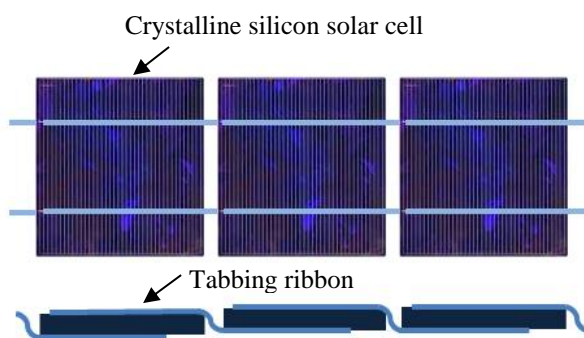
114 2.2 Challenges of conventional interconnection technology 115

116 The manufacture of crystalline silicon solar cells using the conventional form of assembly
117 results in associated challenges which limit the quantity of energy generated as well as
118 imparts the thermo-mechanical reliability of PV modules. These challenges include series
119 resistance, shadowing losses and induced thermo-mechanical stress in the solar cells.

120
121 Series resistance losses are one of the major challenges associated with the manufacture of
122 solar cells in the conventional form. These losses are created due to metallization for contact
123 formation and the subsequent tabbing for current collection. In order to reduce these losses,
124 new concepts are being developed with additional objectives of providing contacts for thinner
125 wafers. This objective is aimed at: reducing material cost, ensuring low-stress interconnection
126 between cells and enabling the ease of modules manufacture [19].

127 Another key challenge of conventional interconnection technology is shadowing losses.
 128 When cells are made wider, thicker interconnection ribbon is required to conduct larger
 129 currents. It is reported in [20] that increase in the width of interconnection ribbon cross-
 130 section increases the shadowing losses proportionally. The thickness of ribbon strip is limited
 131 by built-up stresses in the soldered joint. The differences in coefficient of thermal expansion
 132 between ribbon interconnection materials and silicon account for this stress accumulation [20,
 133 21]. Furthermore, stress occurrence at the edge of the wafers due to bending of the
 134 interconnection ribbon strip which connects the front side with the rear of the neighbouring
 135 wafer [21] impacts the reliability of the assembly. This situation entails that conventional
 136 interconnection technology makes a compromise between width and thickness of ribbon strip.
 137 Apart from shadowing losses, there are also recombination losses which are not influenced by
 138 interconnection technologies. However, reduction of these losses is desirable to enhance solar
 139 cell efficiency. This reduction can be achieved through the use of Laser-Fired Contact (LFC)
 140 process, particularly for the rear surface, to fabricate solar cells with a high quality rear
 141 surface [15, 22].

142 Induced thermo-mechanical stress in the solar cells is another challenge associated with the
 143 manufacture of solar cells in the conventional form. The manufacturing process of
 144 interconnecting wafer-based silicon solar cells involves the use of infra-red (IR) reflow
 145 soldering. The soldering process consists of two phases. These are stringing or tabbing as
 146 well as bussing. The former involves the interconnection of solar cells with each other to
 147 form strings while the later deals with the assembly of the strings of solar cells to form PV
 148 module [23, 24]. However, this interconnection procedure is difficult and the IR soldering
 149 induces high mechanical stress in the solder joint which accelerates fatigue related damage.
 150 Eventually, module failure occurs during field operations thereby halting energy generation.
 151 Figure 2 presents a diagram of solder interconnection between tabbing ribbon and
 152 conventional wafer-based crystalline silicon (c-Si) solar cells while Fig. 3 depicts a schematic
 153 of a typical laminated crystalline Si solar cell showing its cross-section. Figure 4 shows
 154 typical interconnected solar cells with tabbing and bussing ribbons while Fig. 5 shows a
 155 typical PV module with complete interconnected solar cells.



156
 157 Fig. 2. Crystalline silicon solar cells interconnected
 158 in series with tabbing ribbon

Fig. 3. Schematic of cross-section of a typical laminated crystalline Si solar cell.



Fig. 4. Interconnected solar cells with tabbing and bussing ribbons [25]



Fig. 5. PV Module with complete interconnected solar cells [23]

In order to address some of the challenges of crystalline silicon solar cells interconnection using IR soldering, laser soldering technology is used because it offers some advantages. Laser soldering is well controlled and enables selective processing. Additionally, when used for spot soldering, it delivers heat very fast, precisely and efficiently on a small area of the solder interconnection without making physical contact with the brittle crystalline silicon solar cells. Since physical contact during soldering can result in cell breakage, laser soldering has demonstrated potentials of inducing minimal thermo-mechanical stresses on the solder joint as well as less probability of causing cell breakage during manufacture which will increase production yield [26].

2.3 Comparison of different interconnection technologies

In order to address the interconnection challenges, many unconventional PV modules with improved interconnection have been developed. Their interconnect concepts include back contact cells technology. In this technique, the interconnection materials and circuitry are located exclusively behind the cells. Examples include emitter wrap-through (EWT), metallisation wrap-through (MWT) and back-junction back-contact (BJBC). Other cell/module concepts are alternate p- and n-type, honeycomb design (HD), pin up modules (PUM), sliver, spherical and cells with flexible electrode wire grid (Day4 Electrode).

Back contact solar cells which include EWT, MWT and BJBC use in-plane interconnectors for interconnection of neighbouring cells [27]. The advantages of these cells over their conventional counterpart include: possession of reduced stress in the soldered joint, possession of minimal shadowing loss caused by metal grids, provision of more surface area for current generation, optimisation of module efficiency and improvement of aesthetics of the module [20, 28, 29].

Alternate p- and n-type silicon solar cells are bifacial screen-printed cells which use alternating p- and n-type semiconductor devices thereby allowing direct interconnection of equivalent sides on front-to-front and back-to-back of neighbouring cells [30]. The advantages of this solar cell technology compared to their conventional equivalent include

190 simpler interconnection procedure, closer assembly of cells (for aesthetic reasons) and higher
191 yield during module fabrication.

192 Honeycomb design (HD) solar cells are cells made with surface texturing that resembles
193 honeycomb structure. This type of design provides very effective light trapping in the cell by
194 total internal reflection. The honeycomb texturing reduces surface reflection of the solar cells
195 [31,32]. The interconnection of the thin HD crystalline silicon solar cells is achieved through
196 the use of an integrated series-connection structure. The advantage of HD cell concept is that
197 series resistance losses are reduced due to removal of areas with contact resistance which are
198 present in conventional cells.

199 Pin up modules are back-contacted solar cells designed with a structured interconnecting
200 back foil and limited number of holes in the wafer. The holes are used as vias and contain
201 pins serving as interconnection from the front-side metallisation to the interconnection
202 material at the rear [21, 33]. The advantages of Pin up modules over conventional modules
203 include possession of minimal series resistance and shadowing losses.

204 Sliver cells are perfectly bifacial monocrystalline silicon solar cells. These cells are long,
205 narrow, thin and symmetrical in appearance. The technology employed in the fabrication of
206 these cells promotes economy in the usage of silicon materials. A decrease of about 10 to 20
207 times the quantity of silicon used in other conventional technologies is obtainable when sliver
208 cells technology is utilised [34]. The sliver cells are interconnected with two thin, narrow
209 substrate supports to form a conventional solar cell analogue. The cells are thin with
210 collecting junctions on both surfaces and the contacts are on the rear of the cell [35]. The
211 advantage of sliver cells concept is that shadowing losses are minimised compared to
212 conventional crystalline cells.

213 Spherical silicon solar cells capture light from all directions because of the spherical
214 geometric nature of the reception surface. This design feature has the capacity to improve the
215 amount of power the system generates to the maximum [36]. The benefits of spherical solar
216 cells include less silicon usage, lower cost and usable in a variety of applications [37]. The
217 spherical cells are interconnected adjacent to one another to form a mini-module in series
218 which produces a specific constant voltage; and current which may be varied. A key
219 advantage of spherical cells over conventional crystalline cells is that shadowing losses are
220 effectively eliminated.

221 Silicon cells with flexible electrode wire grid (Day4 Electrode) structurally consists of
222 transparent polymeric film, a layer of adhesive and embedded copper wires coated with low
223 melting point alloy [38] which interconnects the cells with copper wires. The copper wires
224 are very tiny and embedded in the transparent film. This arrangement has the advantage of
225 minimal shadowing effect predominant in the conventional crystalline cells.

226 Although IR and laser soldering technology are used in several cell concepts, they are not the
227 only interconnection techniques. [Techniques which include ultrasonic welding \[39\], thermal
228 spraying \[40\] and conductive adhesives \[41\] have been successfully employed.](#) Each of these
229 techniques induces thermo-mechanical stress in the solder joint to some degree. The

230 techniques create series resistance and shadowing losses in the solar cell. Moreover, these
231 techniques induce thermo-mechanical stress in the interconnection joint. The mechanism of
232 thermo-mechanical stress origin is dependent on the difference between solder melting
233 temperature and room temperature. This conveys the concept of homologous temperature of
234 material. Homologous temperature expresses the temperature of a material as a fraction of its
235 melting point using the Kelvin scale. At low homologous temperatures, joint materials of
236 interconnected solar cells are structurally modified and residual intrinsic stresses are induced
237 in the joint. On the other hand, processing temperature for each interconnection technique is
238 different. The typical reflow temperature for tin-silver-copper (SnAgCu) solder used for
239 interconnection of conventional front-to-back cells is about 250 °C [42]. Similarly,
240 processing temperature for laser spot soldering of cells is about 225 °C [26] while for
241 ultrasonic welding, the temperature is about 177 °C [43]. Likewise, the processing
242 temperature for interconnection of cells using thermal arc metal spraying and conductive
243 adhesive is about 150 °C [40] and 125 °C [41] respectively.

244 Interconnection of solar cells results in bonded materials at the interconnection joint. In order
245 to ensure that the bond has adequate strength, the bond is tested to determine its peel force.
246 Peel force is the measure of adhesion strength required to part bonded materials. The
247 interconnection concepts developed and their corresponding interconnection techniques with
248 peel force and residual stress are presented in Table 1. It can be observed in the table that
249 some interconnection concepts have more than one interconnection technique. It therefore
250 serves as a reference guide to PV manufacturers who may be interested in making choices of
251 technique to use when consideration on peel force and induced residual stress in the solder
252 joint are factors.

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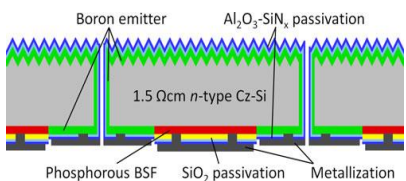
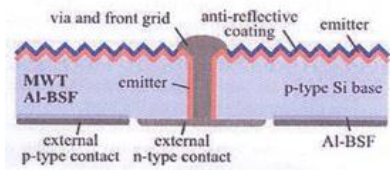
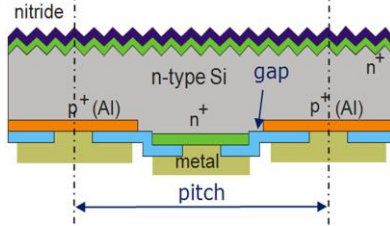
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Table 1: Comparison of different interconnection techniques with peel force and residual stress for various interconnection concepts employed in assembly of crystalline silicon solar cells

Interconnection concept	Inter-connection technique	Peel force (N)	Residual stress (MPa)
 <p>Conventional front-to-back cell interconnection [24].</p> <p>Tabbing ribbon soldered to front and back of cell [25, 26].</p>	IR soldering	2-16 [44]	49-359 [45] (Simulation)
	Laser spot soldering	1-5 [46, 47]	NA
 <p>Back-contact EWT solar cells [48].</p> <p>Hole drilled for vias which allow emitter wrap through from front of the cell to the back surface [27-29, 48, 49].</p>	Laser soldering	1-5 [46,47]	NA
	Conductive adhesive	0.3-1 [50]	15-19.5 [51] (Simulation)
 <p>MWT solar cells [53].</p> <p>Similar to EWT cells but has metal grid contact on the front surface while interconnection pads for both polarities are on the rear surface [52-54].</p>	Laser soldering	1-5 [46, 47]	NA
	Conductive adhesive	0.3-1 [50]	15-19.5 [51] (Simulation)
 <p>BJ-BC solar cells [55]</p> <p>Both emitter and metallisation are located at the rear surface of the cell [55, 56]</p>	IR soldering	2-16 [44]	49-359 [45] (Simulation)

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Table 1 (Continued)

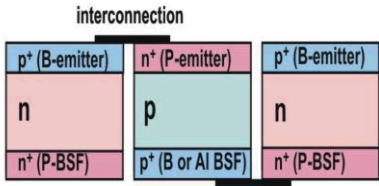
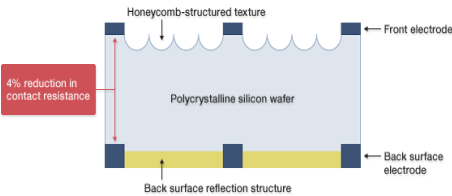
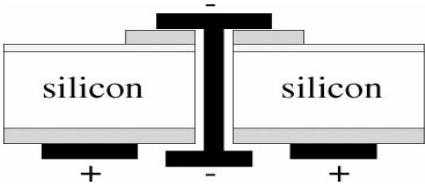
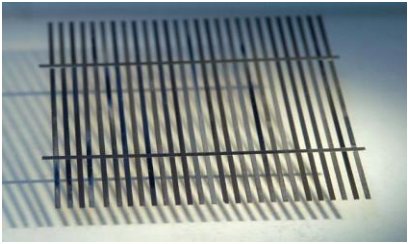
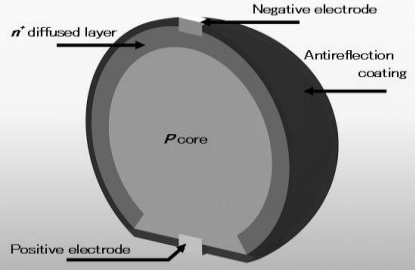
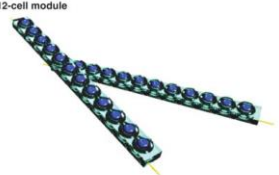
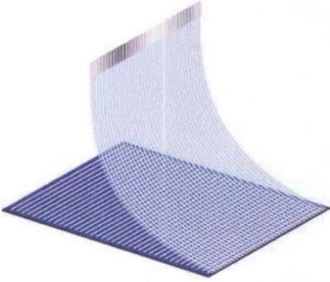
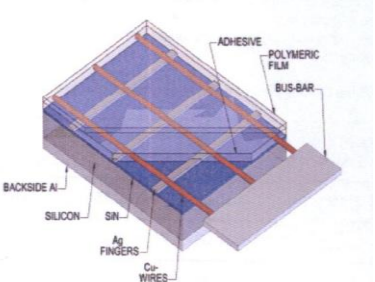
Interconnection concept	Inter-connection technique	Peel force (N)	Residual stress (MPa)
 <p>Alternate p- and n-type silicon solar cells [30].</p> <p>These bifacial cells allow direct interconnection of equivalent sides on front-to-front and back-to-back of neighbouring cells [30].</p>	IR soldering	2-16 [44]	49-359 [45] (Simulation)
 <p>HD solar cell [58]</p> <p>Interconnection of the thin HD cells is achieved through the use of an integrated series-connection structure [31, 32, 57, 58].</p>	IR soldering ----- Conductive adhesive	2-16 [44] ----- 0.3-1 [50]	49-359 [45] (Simulation) ----- 15-19.5 [51] (Simulation)
 <p>PUM Cell [33].</p> <p>Interconnection from the front-side metallisation to the interconnection material at the rear achieved through vias containing pins [33, 59].</p>	IR soldering ----- Thermal arc metal spraying	2-16 [44] ----- NA	49-359 [45] (Simulation) ----- NA
 <p>Sliver cells [34, 35].</p> <p>Cells interconnected by two thin, narrow substrate supports [34, 35].</p>	Solder bumps	1-5 [46, 47]	NA

Table 1 (Continued)

Interconnection concept	Inter-connection technique	Peel force (N)	Residual stress (MPa)
 <p>Spherical cell [36].</p> 	Ultrasonic welding	2-5 [62]	NA
<p>Interconnected spherical cells [37].</p> <p>Cells are interconnected adjacent to one another to form mini-modules which in turn are interconnected by ultrasonic welding [36, 37, 60, 61].</p>			
 <p>Cell with flexible electrode [64].</p> 	Conductive adhesive	0.3-1 [49]	15-19.5 [50] (Simulation)
<p>Cell in contact with electrode [65].</p> <p>Interconnection achieved using flexible Day4 electrode wire grid consisting of transparent polymeric film, a layer of adhesive and embedded copper wires coated with low melting point alloy. The wire grid is glued to the cells using adhesives to obtain interconnection [38, 63-65].</p>			

271 Furthermore, interconnection technologies for silicon solar cells are numerous and have
272 various applications. The conventional interconnection concepts remain dominant while the
273 other concepts are completely unconventional and modest. The review found some concepts
274 which combine conventional with other concepts. For instance, on-laminate laser soldering
275 (OLLS) was developed to combine the reliability potentials of conventional module assembly
276 with the smoothness potential of the process steps in the monolithic module assembly
277 (MMA) [66, 67]. The concept involves interconnecting solar cells on a patterned back sheet
278 foil using conductive adhesives or low melting point solders [68].

279 Table 2 presents a comparison of interconnection technologies employed in the manufacture
280 of silicon solar cells including thin-film silicon solar cells. The index of comparison is cell
281 type, joint type and production status. It can be observed from the table that conventional
282 interconnection technologies for wafer-based silicon solar cells and for thin-film silicon solar
283 cells are the only widespread and commercially available technologies. New concepts used in
284 solar cells interconnection are either partially available or are yet to be commercially
285 available.

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304 Table 2: Comparison of silicon solar cells interconnection technologies in terms of cell type,
 305 joint type and production status

	Cell type	Interconnect technology	Joint type	Production status			
				Widespread	Partially	R & D	
Silicon solar cells	Wafer-based	Conv. c-Si and mc-Si	Ribbon (front-to-back)	Solder joint	✓		
		Alternate p- and n-type	Ribbon (equivalent sides)	Solder joint			✓
		EWT	Edge tab (back contact)	Solder/conductive adhesive joint		✓	
		MWT	Conductive foil/Ribbon	Conductive adhesive/Solder joint		✓	
		EWT, MWT	Bone-shaped interconnector (MMA)	Laser solder joint			✓
		Honeycomb design	Ribbon/Adhesive	Solder/conductive adhesive joint			✓
		PUM	Foils with patterned conductors	Solder/thermal metal spraying			✓
		Sliver	Substrate support bond	Solder joint		✓	
		c-Si and mc-Si	Day4 electrode	Day4 electrode adhesive joint		✓	
		Cz. Si	Spherical	Substrate support bond	Ultrasonic Welded joint		✓
		Thin-film	Conv. a-Si and μ c-Si	Monolithic series	Conductive film bond		

306

307 **3. Interconnection materials and technology reliability challenges of silicon solar cells**

308 Although it is reported in [69] that the reliability status of PV systems is good, even with a
 309 reliable technology there is always room for improvement. With the reported recent cases of
 310 unprecedented failure of PV modules in the tropics, the improvement of reliability of
 311 modules has become essential more so as the improvement will encourage more system
 312 uptake. System's reliability depends to some extent on their cost of manufacture and it is
 313 measured by parameters which include systems performance, availability and degradation
 314 during operation and maintenance (O&M) and predictability [70] as well. It has been widely
 315 reported that the daily thermal cycles which PV modules are subjected to in the field is one of
 316 the causes of degradation experienced by its interconnection. In addition to accelerating
 317 interconnect degradation; the thermal cycling also increases series resistance [71]. As
 318 discussed previously, silicon solar cells are interconnected with one another either by the

319 process of soldering or by the use of electrical conductive adhesive [72]. The reliability
320 challenges of each technique are widely reported by researchers. In this section, this review
321 will present and discuss the challenges associated with these two techniques. It will discuss
322 the reliability of interconnection made using solder in sub-section 3.1 while in sub-section
323 3.2, it will discuss the reliability of interconnection made using electrical conductive
324 adhesives.

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327 3.1 Reliability of solder interconnection in PV modules

328 The key materials used in the assembly of conventional crystalline silicon modules include
329 silicon, glass, copper ribbon, back sheet, encapsulant, bus-bar and solder [24]. A critical part
330 of the module is the solder joint interconnections. They consist of many materials bonded
331 together. The materials bonded together in the joint are the solder, bus-bar, ribbon and the
332 silicon wafer. These materials possess different thermal and mechanical properties. In
333 bonding, the assembly develop thermo-mechanical reliability issues which are caused by
334 differences in the bonded materials' coefficient of thermal expansion (CTE). In PV module
335 solder interconnection, the solder provides a connection between the electrode and ribbon.
336 This connection is the pathway through which current flows from the silicon semiconductor
337 to the ribbon. The PV module temperature varies according to local weather which in turn
338 affects the rate of solder interconnection degradation. In a lifetime prediction modelling
339 analysis [73], Han et al reported that for the same type of Si PV modules located in various
340 weather conditions, lifetime was shortest in a desert followed by those in the tropics.

341

342 Although the use of soldering process in the assembly of solar cells in PV modules has the
343 advantage of yielding products which possess high reliability at minimal production cost, the
344 technology occurs at high temperature with inherent potential to produce shear stress in the
345 silicon wafer. This occurrence which is due to the differences in CTEs of the bonded
346 interconnect materials in the assembly [74] may result in systematic grid finger interruptions
347 at the bus-bar edges [24, 74] and also fatigue damage. In the presence of transients associated
348 with passing clouds and daily thermal cycling, the joints are exposed to fatigue loading which
349 leads to metal segregation, grain boundary coarsening/cracking and increased series
350 resistance and heating [7, 75, 76]. Some approaches have been proposed to either reduce or
351 avoid these reliability issues which have been discussed and presented earlier in
352 unconventional interconnection concepts.

353

354 Interconnection technologies involving the use of laser soldering for interconnecting solar
355 cells have been developed by researchers for various concepts of PV modules. Utilising laser
356 soldering technology for interconnection has the potential to ensure that the joints are highly
357 reliable when compared to conventional soldering technology. This is because laser soldering
358 induces minimal thermal and mechanical stresses in the solder joints. In an experimental
359 investigation [77], Schmidhuber et al reported that peel force in conventional soldered tabs
360 was in the range of 1 to 3 N while that in a laser soldered tabs is about zero. This finding
361 supports the earlier statement that laser soldering has minimal mechanical damage in the
362 solar cell interconnection. Therefore, the adoption and use of laser soldering technology to
363 interconnect crystalline silicon cells need to be explored as a replacement for conventional
364 soldering technology for improved reliability of solder interconnections in crystalline PV
365 modules.

366

367 3.2 Reliability of electrical conductive adhesive interconnection in PV modules

368 The elevated temperature soldering of cells induces stress in the cells. In addition to the
369 induced stress, the solder joints are also stressed and deformed during operations in the field.
370 The deformation of the joints culminates in cell warpage, breakage and ultimately system
371 failure at prolonged operations.

372
373 To avoid this situation, some manufacturers use electrical conductive adhesives in place of
374 solder for the interconnection. The electrical conductive adhesives, which are made of silver-
375 loaded epoxy resins, are being used successfully as an alternative bonding material for solar
376 cells interconnection [78]. The use of conductive adhesives as an alternative to solder has
377 been shown to have minimal change on the mechanical properties of the bonded materials in
378 the joints. Similarly, its use enhances the conductivity of the joint. As this bonding process is
379 carried out at low temperature, it leaves minimal residual stress on the joint with advantage of
380 minimal cell breakage [78, 79]. It is pertinent to note that conductive adhesives can be used
381 for interconnecting both crystalline and thin film solar cells.

382
383 Although the adoption and use of this low temperature bonding technology appear to solve
384 the initial challenge encountered in using soldering process, there are some key reliability
385 challenges associated with modules manufactured using the process during field operations.
386 The adhesives undergo accelerated degradation occasioned by oxidation of the adhesive
387 material. Moreover, the adhesive-to-metal bond, which is the interconnection joint,
388 experience de-bonding [78, 80]. The de-bonding commences with crack initiation and
389 propagation which enables corrosion induced system failure.

390

391 **4. Future R&D challenges and opportunities**

392

393 While several crystalline silicon module concepts have been developed to address the various
394 challenges discussed earlier, there is no single concept that has solved all the challenges.
395 Therefore, opportunities exist for more research and development (R&D) for further
396 improvement of the cells design and manufacture. In this regard, R&D opportunities focussed
397 on series resistance, shadowing and recombination losses as well as induced thermo-
398 mechanical stress are discussed as follows.

399

400 Series resistance losses in a crystalline silicon solar cell have three main causes. The first
401 cause is the current flow through the emitter and base of the solar cell while the second cause
402 is the contact resistance between the metal contact and the silicon. The final cause is the
403 resistance of the top and rear metal contacts. In addition, it is also known that thermal cycling
404 increases series resistance. Considerable R&D is required aimed at reducing series resistance
405 losses through the decrease in metal contact resistivity which can improve energy conversion
406 efficiency of the cells.

407 Shadowing losses result from interconnection ribbons placed on the surface of wafer-based
408 crystalline silicon cells. Their presence on the cell surface occupies precious space thereby
409 preventing power generation by that cell portion. Increase in the width of interconnection
410 ribbon cross-section increases the shadowing losses proportionally. The best situation will be
411 to completely relocate the interconnection to the back of the cell. This desire forms the basis
412 for back contact cell concepts. However, the fabrication challenges associated with these
413 concepts has affected the uptake of the technology. Furthermore, the reliability of these

414 concepts is yet to be proven in long-term field exposure. Thus, the R&D opportunities for
415 reduction of shadowing losses include simplification of fabrication processes and ensuring
416 solar cells developed are durable and reliable.

417

418 Induced thermo-mechanical stress in PV modules is a concern that requires proper attention.
419 Photovoltaic module interconnection consisting of solder joints, ribbon and busbar are found
420 to be the most vulnerable part to degradation and failure. As mentioned earlier, the
421 differences in CTE among these bonded materials and long repeated temperature cycles
422 induce thermo-mechanical strain and stress in the joint. These factors lead to module
423 untimely failure which becomes aggravated in poor solder bonding between ribbon and silver
424 busbar. Concerted R&D is needed for the optimization of the parameter settings involved in
425 manufacture of these modules to improve the reliability of PV module assembly. These
426 parameters are the dimensions of the ribbon, busbar, backsheet and any other critical
427 dimension identified. The application of finite element modelling in the early design stage of
428 PV modules has the potential to predict the response of the assembly to cyclic thermo-
429 mechanical stresses and strains. The techniques could also be used to determine the optimal
430 parameter settings of the control factors in the module assembly. This will enable the
431 determination of an optimal parameter setting of solder joint to improve the thermo-
432 mechanical reliability of PV module assembly. Additionally, more R&D is required for
433 conductive adhesives used for solar cells interconnection in order to improve their durability
434 and reliability.

435

436

437 **5. Summary**

438

439 A review of contacts and interconnection technologies used to assemble crystalline silicon
440 solar cells has been presented and discussed in this paper. The review was extended to
441 include detailed description of the concepts and interconnection technologies employed in the
442 manufacture of unconventional silicon solar cells.

443

444 It was found that the predominant interconnection technology used in the manufacture of
445 wafer-based silicon solar cells involves soldering of ribbon on the surface of cell. This basic
446 technique is shown to be none ideal because the soldering process induces thermo-
447 mechanical stresses in the cells and joints. The review results show that the process of
448 interconnecting ribbon on the front-to-back surface of the cells leads to significant series
449 resistance, shadowing losses. It identifies the technology of laser soldering as one which is
450 poised to produce high reliability interconnection joints in the module. The capacity to heat
451 only very small area of the ribbon placed on the cell enables the laser technology to induce
452 minimal stress on the cell and joints after soldering and consequently produces quality
453 assembly. On the other hand, it was found that adhesive-to-metal bond experiences
454 substantial crack initiation and propagation which enables corrosion induced system failure.
455 More review results indicate that the concepts developed for unconventional solar cell (to
456 address the current reliability issues in the manufacture of PV modules) are yet to attain
457 popular uptake because of lack of track record, major changes in tooling and manufacturing
458 facilities as well as their attendant cost.

459

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464

465 **References**

466
467 [1] Jeong J, Park N, Hong W. Analysis for the degradation mechanism of photovoltaic ribbon wire under
468 thermal cycling. In: Photovoltaic Specialists Conference (PVSC), 2011 37th IEEE, Seattle, WA; 2011.
469 [2] Miles RW. Photovoltaic solar cells: Choice of materials and production methods. *Vacuum* 2006;
470 **80**(10): 1090-97.
471 [3] Saga T. Advances in crystalline silicon solar cell technology for industrial mass production. *NPG Asia*
472 *Materials* 2010;82, **2**(3): 96-102.
473 [4] Gress PJ, Widenborg PI, Varlamov S, Aberle AG. Wire bonding as a cell interconnection technique
474 for polycrystalline silicon thin-film solar cells on glass. *Progress in Photovoltaics: Research and*
475 *Applications* 2010; **18**: 221-28.
476 [5] Klengel R, Petzold M, Schade D, Sykes B. Improved testing of soldered busbar interconnects on
477 silicon solar cells. In: *Microelectronics and Packaging Conference (EMPC)*, Brighton, UK; 2011.
478 [6] Sakamoto S, Kobayashi T, Nonomura S. Epidemiological analysis of degradation in silicon
479 photovoltaic modules. *Japanese Journal of Applied Physics* 2012; **51**: 1-4.
480 [7] McCluskey FP. Reliability modeling for photovoltaic modules. In: *Photovoltaic Module Reliability*
481 *Workshop*, Denver, Colorado; 2010.
482 [8] Jeong J, Park N, Han C. Field failure mechanism study of solder interconnection for crystalline silicon
483 photovoltaic module. *Microelectronics Reliability* 2012; **52**(9–10): 2326-30.
484 [9] Skoczek A, Sample T, Dunlop ED. The results of performance measurements of field-aged crystalline
485 silicon photovoltaic modules. *Progress in Photovoltaics: Research and Applications*, 2009; **17**(4): 227-
486 40.
487 [10] Granata JE, Boyson WE, Kratochvil JA, Quitana MA. Long-Term Performance and Reliability
488 Assessment of 8 PV Arrays at Sandia National Laboratories. In: *Photovoltaic Specialist Conference*
489 *(PVSC)*, 34th IEEE. Philadelphia, PA; 2009.
490 [11] Campeau Z, Anderson M, Hasselbrink E, Kavulak D, Shen Y-C, Lacerda R, Terao A, Caldwell S,
491 Defreitas Z, Leonard L, Mikofski M, DeGraaff D, Budiman A. SunPower® Module Degradation Rate.
492 SunPower Corporation 2013; 1-61.
493 [12] Nijs J. Photovoltaic Solar Energy : present and future, in Aurelio Peccei Lectures. The Royal Flemish
494 Academy of Belgium of Sciences and Arts 2009; 1-103.
495 [13] Burger B, Kiefer K, Kost C, Nold S, Philipps S, Preu R, et al. *Photovoltaics Report*. Fraunhofer
496 Institute for Solar Energy Systems ISE: Freiburg, Germany; 2014. 1-42.
497 [14] Tsunomura Y, Yoshimine Y, Taguchi M, Baba T, Kinoshita T, Kanno H, et al, Twenty-two percent
498 efficiency HIT solar cell. *Solar Energy Materials and Solar Cells* 2009; **93**(6–7): 670-73.
499 [15] Mette A. New concepts for front side metallization of industrial silicon solar cells. In: Faculty of
500 Applied Sciences, Albert Ludwig University of Freiburg in the Breisgau, Germany Breisgau; 2007.
501 241.
502 [16] Glunz SW, Preu R, Biro D. Crystalline silicon solar cells: State-of-the-art and future developments.
503 *Comprehensive Renewable Energy* 2012; **1**: p. 353-87.
504 [17] Schubert G, Huster F, Fath P. Physical understanding of printed thick-film front contacts of crystalline
505 Si solar cells—Review of existing models and recent developments. *Solar Energy Materials and Solar*
506 *Cells* 2006; **90**(18–19): p. 3399-406.
507 [18] Cuddalorepatta G, Dasgupta A, Sealing S, Moyer J, Tolliver T, Loman J. Durability of Pb-free solder
508 between copper interconnect and silicon in photovoltaic cells. *Progress in photovoltaics: research and*
509 *applications* 2010; **18**(3): p. 168-82.
510 [19] Löffler J, Wipliez L, Soppe W, Keijzer M, Bosman J, Lamers M, et al. Laser processing for advanced
511 solar cells. In: *Proceedings of LPM - the 11th International Symposium on Laser Precision*
512 *Microfabrication*, Stuttgart, Germany; 2010.
513 [20] Kerschaver EV, Beaucarne G. Back-contact solar cells: a review. *Progress in Photovoltaics: Research*
514 *and Applications* 2010; **14**(2): 107-23.

- 515 [21] Bultman JH, Weeber AW, Brieko MW, Hoornstra J, Burgers AR, Dijkstra JA, et al. Pin up module: a
516 design for higher efficiency, easy module manufacturing and attractive appearance,
517 <<http://www.ecn.nl/docs/library/report/2000/rx00010.pdf>>; 2012 [accessed 26.11.2012].
- 518 [22] Zeman M. Heterojunction silicon based solar cells. 2009, Delft University of Technology Database,
519 Netherlands,
520 <[http://www.jointsolarpanel.nl/fileadmin/jointsolarpanel/user/documents/seminar2009/4_Miro_Zeman](http://www.jointsolarpanel.nl/fileadmin/jointsolarpanel/user/documents/seminar2009/4_Miro_Zeman_Delft_University_of_Technology.pdf)
521 <[_Delft_University_of_Technology.pdf](http://www.jointsolarpanel.nl/fileadmin/jointsolarpanel/user/documents/seminar2009/4_Miro_Zeman_Delft_University_of_Technology.pdf)> ; 2012 [accessed 12.12.2012].
- 522 [23] Chen YM, Chiu Y, Wu H. Improved testing of soldered interconnects quality on silicon solar cell.
523 Global Perspective on Engineering Management 2012; **1**(2): 51-58.
- 524 [24] Grunow P. Soldering of crystalline silicon modules: losses, reliability and improvements. In:
525 Proceedings of the 2nd Workshop on Metallization for Crystalline Silicon Solar Cells, Constance,
526 Germany; 2010.
- 527 [25] Helmers H, Oliva E, Bronner W, Dimroth F, Bett AW. Processing techniques for monolithic
528 interconnection of solar cells at wafer level. IEEE Transactions on electron devices 2010; **57**(12):
529 3355-60.
- 530 [26] Wirth H. Lasers in wafer-based PV module production. Laser Technik Journal 2010; **7**(4): 36-38.
- 531 [27] Eitner U, Altermatt PP, Kontges M, Meyer R, Brendel R. A modeling approach to the optimization of
532 interconnects for back contact cells by thermomechanical simulations of photovoltaic modules. In 23rd
533 European Photovoltaic Solar Energy Conference, Valencia, Spain; 2008.
- 534 [28] Choi J, Lee J, Kim S, Park H, Kim K, Lee W. Industrial development of silicon hetero-junction back
535 contact solar cells. In: Photovoltaic Specialists Conference (PVSC), 38th IEEE, Austin, TX.; 2012.
536 001023 - 25.
- 537 [29] Kim DS, Meemongkolkiat V, Ebong A, Rounsaville B, Upadhyaya V, Das A, et al. 2D-modeling and
538 development of interdigitated back contact solar cells on low-cost substrates. In Photovoltaic Energy
539 Conversion, Conference Record of the IEEE 4th World Conference, Waikoloa, HI.; 2006. p. 1417 - 20.
- 540 [30] Buck T, Kopecek R, Libal J, Petres R, Peter K, Rover I, et al. Large area screen printed n-type mc-si
541 solar cells with b-emitter: efficiencies close to 15% and innovative module interconnection. In:
542 Photovoltaic Energy Conversion, Conference Record of the IEEE 4th World Conference. Waikoloa,
543 HI.; 2006. p. 1060 - 63.
- 544 [31] Huang CK, Sun KW, Chang WL. Efficiency enhancement of silicon solar cells using a nano-scale
545 honeycomb broadband anti-reflection structure. Optics Express 2012; **20**(S1): p. A85-93.
- 546 [32] Zhao J, Wang A, Campbell P, Green MA. A 19.8% efficient honeycomb multicrystalline silicon solar
547 cell with improved light trapping. IEEE Transactions on electron devices 1999; **46**(10): p. 1978-83.
- 548 [33] Bultman JH, Brieko MW, Burgers AR, Hoornstra J, Tip AC, Weeber AW, Interconnection through
549 vias for improved efficiency and easy module manufacturing of crystalline silicon solar cells. Solar
550 Energy Materials & Solar Cells 2001; **65**: 339-45.
- 551 [34] Franklin E, Everett V, Blakers A, Weber K. Sliver solar cells: high-efficiency, low-cost PV technology.
552 Advances in OptoElectronics 2007; 1-9.
- 553 [35] Stocks MJ, Weber KJ, Blakers AW. Fabrication of solar cells using the epilift technique. In: 3rd World
554 Conference of Photovoltaic Solar Energy Conversion, Osaka, Japan; 2003. 1-4.
- 555 [36] Taira K, Inagawa I, Omura E, Imoto S, Nakata J. Proprietary spherar® technology for sustainable
556 living in the 21st century. In: Proceedings of ECOpole, Wilhelms Hill at Uroczyisko in Piechowice, PL;
557 2008.
- 558 [37] Taira K. Spherar cells save on silicon, capture light from all paths. Journal of the Electronics Industry
559 2007; 26-27.
- 560 [38] Schneider A, Rubin L, Rubin G. Solar cell efficiency improvement by new metallization techniques –
561 The DAY4™ electrode concept. In: Photovoltaic Energy Conversion, Conference Record of the IEEE
562 4th World Conference, Waikoloa, HI.; 2006.
- 563 [39] Brdason Ultrasonics, Ultrasonic Welding Machine for Solar Panel,
564 <<http://www.brdason.com/En/ProductView.asp?ID=15>>; [accessed 21.04.2015].
- 565 [40] Praxair Surface Technologies. Thermal Spray Process.
566 <[http://www.praxairsurfacetechologies.com/na/us/pst/pst.nsf/0/52E8B4E608B4BB04852576A50056](http://www.praxairsurfacetechologies.com/na/us/pst/pst.nsf/0/52E8B4E608B4BB04852576A50056FB73?OpenDocument)
567 <[FB73?OpenDocument](http://www.praxairsurfacetechologies.com/na/us/pst/pst.nsf/0/52E8B4E608B4BB04852576A50056FB73?OpenDocument)>; [accessed 21.01.2015].
- 568 [41] Eikelboom DWK, Burgers AR, Goris MJAA, Manshanden P, Schönecker A, Wyers GP. Conductive
569 Adhesives for Interconnection of Busbarless Emitter Wrap-Through Solar Cells on a Structured Metal
570 Foil. <<http://www.ecn.nl/docs/library/report/2001/rx01016.pdf>>; 2001 [accessed 22.01.2015].
- 571 [42] Anguiano C, Félix M, Medel A, Bravo M, Salazar D, Márquez H. Study of heating capacity of focused
572 IR light soldering systems. Optics Express 2013; **21**(20): 23851-65.

- 573 [43] Harman GG, Albers J. The Ultrasonic Welding Mechanism as Applied to Aluminum- and Gold-Wire
574 Bonding in Microelectronics. *IEEE Transactions on Parts, Hybrids, and Packaging* 1977; 13(4): 406-
575 12.
- 576 [44] Eitner U, Rendler LC. Peel Testing of Ribbons on Solar Cells at Different Angles - Consistent
577 Comparison by Using Adhesives Fracture Energies. In: 29th European PV Solar Energy Conference
578 and Exhibition, Amsterdam, The Netherlands; 2014.
- 579 [45] Novotný M, Jakubka L, Cejtchaml P, Szendiuch I. Thermomechanical stressing of solar cells. In: 7th.
580 Internal Conference on Thermal, Mechanical and Multiphysics Simulation and Experiments in Micro-
581 Electronics and Micro-Systems, EuroSimE, Como, near Milan Italy, 2006.
- 582 [46] F. Schmitt, A. Prießner, B. Krämer and A. Gillner. Laser Joining Photovoltaic Modules. *Industrial*
583 *Laser Solutions for Manufacturing*, <[http://www.industrial-lasers.com/articles/print/volume-23/issue-](http://www.industrial-lasers.com/articles/print/volume-23/issue-6/features/application-report/laser-joining-photovoltaic-modules.html)
584 [6/features/application-report/laser-joining-photovoltaic-modules.html](http://www.industrial-lasers.com/articles/print/volume-23/issue-6/features/application-report/laser-joining-photovoltaic-modules.html)>; 2008 [accessed 12.04.2015].
- 585 [47] Schmidhuber H, Klappert S, Stollhof J, Erfurt G, Eberspächer M, Preu R. Laser Soldering – A
586 Technology for Better Contacts. In: 20th European Photovoltaic Solar Energy Conference, Barcelona,
587 Spain; 2005, p. 1997-2000.
- 588 [48] Kiefer F, Ulzhofer C, Brendemuhl T, Harder NP, Brendel R, Mertens V, et al. High efficiency n-type
589 emitter-wrap-through silicon solar cells. *IEEE Journal of photovoltaics* 2011; 1(1): 49-53.
- 590 [49] Ulzhofer C, Altermatt PP, Harder NP, Brendel R. Loss analysis of emitter-wrap-through silicon solar
591 cells by means of experiment and three-dimensional device modelling. *Journal of applied physics*
592 2010; **107**(104509): p. 104509-1 -12.
- 593 [50] Bennett I, Geerligs B, Olson C, Goris M. Compatibility of copper-electroplated cells with metal wrap-
594 through module materials, *Photovoltaics International*,
595 <http://www.sustainablepv.eu/fileadmin/sustainablepv/user/PVI21_Paper_08_ECN_Modules_v4.pdf>;
596 2013 [accessed 12.04.2015].
- 597 [51] Hasan K. Thermal Deformation Analysis of Tabbed Solar Cells Using Solder Alloy and Conductive
598 Film, <<http://www.eng.hokudai.ac.jp/e3/alumni/files/abstract/m244.pdf>>; 2014 [accessed 13.04.2015].
- 599 [52] Reitenbach V, Spitz M, Drew A, Weib M, Chighali EO, Thaidigsmann B, et al. Process
600 characterisation of MWT solar cells – A new method to analyse via contacts. In: 27th European
601 Photovoltaic Solar Energy Conference and Exhibition, Frankfurt, Germany; 2012. p. 1335 - 38.
- 602 [53] Lohmüller E, Thaidigsmann B, Werner S, Clement F, Wolf A, Biro D, et al. Evaluation of via pastes
603 for p- and n-type metal wrap through (MWT) solar cells. In: The 27th EU PVSEC, Frankfurt,
604 Germany; 2012, 1-6.
- 605 [54] Kraemer F, Wiese S, Peter EB, Seib J. Mechanical problems of novel back contact solar modules,
606 *Microelectronics Reliability* 2013, **53**(8): p. 1095–100.
- 607 [55] Gong C, Singh S, Robbelein J, Posthuma N, Van Kerschaver E, Poortmans J, et al. High efficient n-
608 type back-junction back-contact silicon solar cells with screen-printed Al-alloyed emitter and effective
609 emitter passivation study. *Progress in Photovoltaics: Research and Applications* 2011; **19**(7): p. 781-6.
- 610 [56] Mangernæs K. Back-contacted back-junction silicon solar cells. Department of Physics, Faculty of
611 Mathematics and Natural Sciences, University of Oslo, Oslo, Norway; 2010. p. 182.
- 612 [57] Wohlgenuth J, Shea SP. Large-scale PV module manufacturing using ultra-thin polycrystalline silicon
613 solar cells - Annual Subcontract Report. National Renewable Energy Laboratory, Golden, Colorado;
614 2004. 1-55.
- 615 [58] Mitsubishi Electric, Polycrystalline silicon photovoltaic (PV) cell,
616 <<http://www.mitsubishielectric.com/company/rd/research/highlight/infra/crystal.html>>; 2009 [accessed
617 28.02.2013].
- 618 [59] Broek KM, Jong PC, Kloos MJH, Nieuwenhof MACJ, Bots TL, Meuwissen MHH, et al. Testing
619 interconnections using conductive adhesives for application in PV modules. In: 21st European
620 Photovoltaic Solar Energy Conference, Dresden, Germany; 2006.
- 621 [60] Murozono M. Specifications of spherical silicon solar cells, Clean Venture 21 Corp., Kyoto, Japan,
622 <<http://www.cv21.co.jp/en/cata.php>>; 2008 [accessed 1.3.2013].
- 623 [61] Nakata J. Spherical Solar Cells Solve Issue of 3-D Sunlight Reception. *Asia Electronics Industry* 2003;
624 43-48.
- 625 [62] Rubin L, Schneider A. Interconnection technology for conventional and concentrator modules (solar
626 cells). In: Lasers and Electro-Optics Society, LEOS, The 20th Annual Meeting of the IEEE. Lake
627 Buena Vista, FL.; 2007.
- 628 [63] Heimann M, Klaerner P, Luechinger C, Mette A, Mueller JW, Traeger M, Barthel T, Valentin O,
629 Wawer P. Ultrasonic Bonding of Aluminum Ribbons to Interconnect High-Efficiency Crystalline-
630 Silicon Solar Cells, *Energy Procedia* 2012; **27**: 670 – 675.
- 631 [64] Day4 Electrode, Leading Edge Solar Electric Technology, Day4 Energy Inc., <<http://libra->
632 [energy.net/attachments/article/89/Day4%20Electrode.pdf](http://libra-energy.net/attachments/article/89/Day4%20Electrode.pdf)> 2013 [accessed 31.1.2013].

- 633 [65] Schneider A, Rubin L, Rubin G, Ospov A, Smirnov A, Antipov P. A new approach in solar cell module
634 interconnection technique resulting in 5-10% higher PV module power output. In: Photovoltaic energy
635 conversion, Conference Record of the IEEE 4th World Conference, Waikoloa, HI.; 2006.
- 636 [66] Köntges M, Gast M, Brendel R, Meyer R, Giegrich A, Merz P. A novel photovoltaic-module assembly
637 system for back contact solar cells using laser soldering technique. In: 23rd European Photovoltaic
638 Solar Energy Conference and Exhibition, Valencia, Spain; 2008.
- 639 [67] Gast M, Köntges M, Brendel R. Lead-free on-laminate laser soldering: a new module assembling
640 concept. *Progress in Photovoltaics: Research and Applications* 2008; **16**(2): 151-7.
- 641 [68] Niyibizi A, Ikua BW, Kioni PN, Kihato PK. Laser material processing in crystalline silicon
642 photovoltaics. In: Mechanical Engineering Conference on Sustainable Research and Innovation, Thika,
643 Kenya; 2012.
- 644 [69] Wohlgemuth JH. Reliability of PV systems. In: Reliability of Photovoltaic Cells, Modules,
645 Components, and Systems, Proceedings of SPIE. SPIE Digital Library; 2008.
- 646 [70] Kurtz S, Granata J, Quintana M. Photovoltaic reliability R&D toward a solar-powered world. In:
647 Reliability of Photovoltaic Cells, Modules, Components, and Systems II, Society of Photographic
648 Instrumentation Engineers (SPIE), San Diego, California; 2009.
- 649 [71] Radue C, Van Dyk EE. A comparison of degradation in three amorphous silicon PV module
650 technologies. *Solar Energy Materials and Solar Cells* 2010; **94**(3): 617-22.
- 651 [72] Zemen Y, Prewitz T, Geipel T, Pingel S, Berghold J. The impact of yield strength of the interconnector
652 on the internal stress of the solar cell within a module. In: 5th World Conference on Photovoltaic
653 Energy Conversion, Valencia, Spain; 2010.
- 654 [73] Han C, Park N, Jeong J. Lifetime Prediction of Silicon PV Module Ribbon Wire in Three Local
655 Weathers. In: PV Module Reliability Workshop, Golden, CO. USA; 2012. p307-1
- 656 [74] Wendt J, Trager M, Mette M, Pfennig A, Jackel B. The link between mechanical stress induced by
657 soldering and micro damages in silicon solar cells. In: 24th European Photovoltaic Solar Energy
658 Conference, Hamburg, Germany; 2009.
- 659 [75] Dhere NG. Reliability of pv modules and balance-of-system components. In: Photovoltaic Specialists
660 Conference, Conference Record of the Thirty-first IEEE; 2005.
- 661 [76] Quintana MA, King DL, McMahon TJ, Osterwald CR. Commonly observed degradation in field-aged
662 photovoltaic modules. In: Photovoltaic Specialists Conference, Conference Record of the Twenty-
663 Ninth IEEE; 2002.
- 664 [77] Schmidhuber H, Klappert S, Stollhof J, Erfurt G, Eberspächer M, Preu R. Laser soldering - A
665 technology for better contacts? In: Proceedings of the 20th European Photovoltaic Solar Energy
666 Conference, Barcelona, Spain; 2005. 1997-2000.
- 667 [78] Eikelboom DWK, Bultman JH, Schonecker A, Meuwissen MHH, Van den Nieuwenhof MAJC, Meier
668 DL. Conductive adhesives for low-stress interconnection of thin back-contact solar cells. In:
669 Photovoltaic Specialists Conference 2002, Conference Record of the Twenty-Ninth IEEE; 2002.
- 670 [79] Hsieh HH, Lee WK, Chang TC, His CS. Photovoltaic modules of crystalline solar cells using a new
671 type assembly structure. In Microsystems Packaging Assembly and Circuits Technology Conference
672 (IMPACT), 2010 5th International, Taipei; 2010.
- 673 [80] Wells R, Francis M. High reliability of conductive adhesives for thin-film interconnect, in Southeast
674 Asia Global Solar Technology. Trafalgar Publications Ltd, Bournemouth, United Kingdom; 2011. 6-
675 10.

676

677